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REMARKS

This application is a division of 09/219,597, filed to pursue the subject matter of nonelected claims 17-31 from the parent case. Claims 1-16 and 32-39 have been cancelled by the present amendment. The claims now in issue are 17-31, with claim 17 being the sole independent claim.

The title of the invention has been amended to reflect more clearly the subject matter of the present claims.

Accompanying the filing of this Preliminary Amendment and new divisional application are a substitute specification and a marked-up copy of the specification as originally filed in the parent case. This substitute specification is substantially identical to the one previously filed in the parent application in response to a requirement set forth by the Examiner in the Office Action dated December 17, 1999 (paper 5). Additional changes have been made only to include continuing data and present a new title to reflect more clearly the subject matter of the present claims. No new matter has been added.

Since the present application is a division of 09/219,597, their specifications should be identical. This substitute specification will eliminate inconsistencies in the text of any patents that issue from these applications.

Consideration of the present claims and passage to issue are respectfully requested.

Applicants' undersigned attorney may be reached in our New York office by telephone at (212) 218-2100. All correspondence should continue to be directed to our below-listed address.

Respectfully submitted,



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PHOTOVOLTAIC ELEMENT MODULE AND ITS PRODUCTION METHOD,  
AND NON-CONTACT TREATMENT METHOD

BACKGROUND OF THE INVENTION

5 Field of the Invention

The present invention relates to a photovoltaic element module and its production method, and a non-contact treatment method, and more specifically to a photovoltaic element module comprising a plurality of electrically connected photovoltaic elements and a method of producing this module.

Related Background Art

10 The problem of <sup>the escalating</sup> global warming caused by the greenhouse effect, that is, an increase in <sup>the amount of</sup>  $\text{CO}_2$  [becomes] <sup>in the</sup> atmosphere, <sup>has produced</sup> [larger, and therefore there is] a growing demand for the development of a clean energy source that does not discharge  $\text{CO}_2$ . One of such energy sources is nuclear power generation. Nuclear power generation, however, has many problems to solve, such as radioactive wastes, so a safer clean energy source is desired. Of the expected clean energy sources, solar cells (photovoltaic elements) are gathering much attention due to their cleanness, safety, and easy handling.

25 At present, the solar cells are roughly classified into a crystal type using single-crystal or polycrystal silicon, an amorphous type using amorphous silicon, and a compound semiconductor type. Of these solar cells,

Continuing data: This application is a division of application number 09/219,597, filed on December 23, 1998.



the amorphous type is highly expected. That is, despite its conversion efficiency <sup>being</sup> lower than that of the crystal type solar cell, the amorphous silicon solar cell has excellent characteristics that are absent from the crystal type solar cell. For example, it can operate in the form of a film because the area of the amorphous type solar cell can be easily increased <sup>also, it</sup> and has a large photoabsorption coefficient.

One of the reasons for <sup>a slow dissemination</sup> [the delayed diffusion] of solar cells <sup>they have drawn</sup> despite the attention [being paid to them] is their high costs. Various methods have been examined to reduce the production costs of solar cells. The representative approaches include:

(1) Reduction of the production costs of a photoelectric conversion layer,

(2) Efficient utilization of an electric power generating region,

<sup>reducing</sup> (3) Reduction of the number of connections <sup>and</sup> thus connection material [costs] and labor costs [for the connections], and

(4) Reduction of the use amount of covering materials and the material costs.

Of these approaches, the present invention particularly relates to the above point (3). The solar cell

connection step is complicated and requires high reliability <sup>however</sup> [while it required] for simplification <sup>and</sup> cost reduction, reduction of the number of parts, <sup>as well as the</sup> [and] an <sup>optimal</sup>

*production* mass-productive connection method *assisted* [by automatization] and high speed treatment. *is required*

Figs. 11A and 11B are schematic views showing an example of a photovoltaic element which is disclosed in, for example, Japanese Patent Application Laid-Open No. 8-139349 and which has been investigated by the inventors. Fig. 11A is a plan view of the photovoltaic element as seen from its light-receiving surface side, and Fig. 11B is a sectional view of the photovoltaic element shown in Fig. 11A, which is taken along the line 11B-11B in Fig. 11A.

A photovoltaic element 600 shown in Fig. 11, is produced by sequentially stacking a lower electrode layer 603, a semiconductor layer 604, and an upper electrode layer 605 on a conductive substrate 602 of, for example, stainless steel.

The upper electrode layer 605 comprises a transparent conductive film such as of indium oxide or indium tin oxide (ITO) and operates as both a reflection-preventing means and a current-collecting means.

A part of the transparent conductive film is linearly removed at a portion as shown by 601 (an etching line) in Fig. 11A by using screen printing or other methods of applying etching paste containing  $\text{FeCl}_3$  or  $\text{AlCl}_3$  to the film and heating it. A part of the transparent electrode film is removed in order to

prevent a short circuit from occurring between the substrate 602 and the upper electrode layer 605 when the outer circumference of the photovoltaic element is cut.

5           In addition, a current-collecting electrode 606 is formed on the surface of the upper electrode layer 605 to efficiently collect generated power. The current-collecting electrode 606 is formed by adhering a metal wire coated with the thin layer of a conductive  
10           adhesive (for example, a copper wire coated with a carbon paste) to the upper electrode layer 605 in order to obtain electric power generated in the semiconductor layer without loss. The copper wire is used in order to reduce power loss, and may be replaced by another  
15           highly conductive material.

          Furthermore, a conductive foil 607 is provided as a further current-collecting electrode in addition to the current-collecting electrode 606. An insulating member 608 is provided under the conductive foil 607 to  
20           ensure the insulation provided by the etching line portion, the performance of which cannot be guaranteed.

          In the photovoltaic element 600, the metal foil 607 and the substrate 602 function, respectively, as terminals of a positive and a negative electrodes to  
25           provide electric power.

          It is difficult, however, for this photovoltaic element to be directly used for electric power

generation. Since the single photovoltaic element normally generates excessively low power, a plurality of photovoltaic elements must be connected in series or parallel to provide a desired voltage and current.

5        Fig. 11C is a plan view showing an example of series-connected photovoltaic elements (in the case of two series). In this figure, the conductive foil 607 of one photovoltaic element is electrically connected in series to the substrate 602 of another adjacent  
10 photovoltaic element by using a connection member 611. Solder is used for the connection and the series connection is completed by carrying out cleaning with a solvent such as MEK (methylethylketone) after soldering.

15        The conventional method of connecting photovoltaic elements to each other, however, has the following problems.

(1) To fix the conductive foil to the metal substrate by using solder, a part of the substrate must  
20 be heated to melt and fix the solder. The heat, however, is transferred through the thermally conductive metal substrate, and the semiconductor layer may degraded <sup>y</sup> over a wide area <sup>working</sup> [to degrade] their specific characteristics. In addition, defects may occur in the  
25 semiconductor layer depending on the heating temperature or time, thereby reducing the yield.

(2) The heating for melting and fixing the solder

may degrade the conductive adhesive provided on the semiconductor element to reduce the adhesion strength and electric conductivity, thereby reducing reliability.

5 (3) Since the solder must be melted, at least about ten seconds are required to heat and cool it, thereby <sup>negatively affecting</sup> ~~reducing~~ mass-productivity.

(4) If an automatic machine is used for mass production, it is difficult to control the temperature  
10 [so as] to achieve uniform soldering and to control the tip of a soldering iron. Thus, automation is difficult.

(5) Even when the solvent, such as MEK, is used to wipe off the excess solder, fluxes adhering to the  
15 substrate cannot be easily removed to cause rust under high-temperature and high-humidity conditions. Consequently, the covering material of the solar cell may be peeled off.

<sup>using a</sup>  
(6) [The use of the] soldering iron for connections  
20 may produce solder residue to reduce the yield. For example, the solder residue may penetrate between the adjacent photovoltaic elements connected in series to cause a short circuit therebetween.

On the other hand, the non-contact treatment  
25 method utilizing radiation of laser light [or] halogen light or electromagnetic waves is widely used in the processing treatment for materials, such as etching.



welding or cutting or in thermal treatment for semiconductor materials. Such a method can more or less solve the problems of the connections using solder.

5 It is important for the non-contact treatment, however, to efficiently absorb light, heat, or electromagnetic waves. When, for example, a material such as gold, silver, copper, or aluminum is used which are frequently used for electrodes for electric parts, 10 in particular, photovoltaic elements, these materials have a high surface reflectance with respect to the laser light and therefore exhibit a lower efficiency of absorbing energy. Thus, the idea for improving the absorption efficiency of energy is required. Also, a 15 method of improving the absorption efficiency of energy is required that can increase the efficiency of energy absorption without the need for additional steps and that enables stable and high speed treatment.

## 20 SUMMARY OF THE INVENTION

It is an object of the present invention to solve the above problems in order to provide a photovoltaic element connection method that is reliable and easy to automate.

25 It is another object of the present invention to provide a photovoltaic element connection method and a laser treatment method that enables stable and high

speed treatment and that utilizes an energy-absorbing medium, and after treatment, the medium does not remain on the treated surface.

The present invention solves the above problems [at a time] to achieve the above objects. The present invention provides a photovoltaic element module comprising at least two photovoltaic elements electrically connected to each other, wherein a medium capable of absorbing at least 10% or more of a light having a wavelength of 0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$  is provided on an electric connection portion of the photovoltaic element.

In addition, the present invention provides a method of producing a photovoltaic module, which comprises [a step of] electrically connecting at least two photovoltaic elements to each other, wherein [the] [step is] a step of providing on a part of a first photovoltaic element a medium capable of absorbing at least 10% or more of a light having a wavelength of 0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$  and then irradiating the medium with the laser beam of wavelength 0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$  to electrically connect the first and second photovoltaic elements to each other.

Furthermore, the present invention provides a method of producing a photovoltaic module, which comprises [a step of] electrically connecting at least two photovoltaic elements to each other, wherein each

of the photovoltaic element has at least a conductive substrate, a semiconductor layer, and a light-transmissive electrode, and wherein [the step is a step] [of] electrically connecting the conductive substrate of  
5 a first photovoltaic element and the light-transmissive electrode of a second photovoltaic element to each other <sup>is done</sup> by laser welding.

Moreover, the present invention provides a non-contact treatment method of carrying out treatment by  
10 using an energy supply means for applying energy, which comprises placing a non-adhering medium capable of absorbing the energy on a material to be treated and irradiating the non-adhering medium with [the] energy.

Moreover, the present invention provides a method  
15 of producing a photovoltaic module, which comprises [a step of] electrically connecting at least two photovoltaic elements to each other, wherein [the step is a step of] <sup>is placed on</sup> placing a non-adhering medium capable of absorbing the energy on a part of a first photovoltaic  
20 element and <sup>is irradiated</sup> [irradiating] the medium with energy to electrically connect the first photovoltaic element and a second photovoltaic element to each other.

#### BRIEF DESCRIPTION OF THE DRAWINGS

25 Figs. 1A and 1B are schematic views showing an appearance of a photovoltaic element module according to Example 1 of the present invention. Fig. 1A is a



plan view of the photovoltaic element as seen from its light-receiving surface side, and Fig. 1B is a sectional view of the photovoltaic element shown in Fig. 1A, which is taken along the line 1B-1B in Fig. 1A;

Fig. 2A is a plan view of two series-connected photovoltaic elements, each of which is shown in Figs. 1A and 1B, as seen from their light-receiving surface side. Fig. 2B is an enlarged view of the series-connected portion in Fig. 2A, and Fig. 2C is a sectional view of the portion as shown in Fig. 2B;

Figs. 3A and 3B are schematic views showing an appearance of a photovoltaic element module according to Example 2 of the present invention. Fig. 3A is a plan view of the photovoltaic element as seen from its light-receiving surface side, and Fig. 3B is a sectional view of the photovoltaic element shown in Fig. 3A, which is taken along the line 3B-3B in Fig. 3A;

Fig. 4A is a plan view of two series-connected photovoltaic elements, each of which is shown in Figs. 3A and 3B, as seen from their light-receiving surface side. Fig. 4B is an enlarged view of the series-connected portion in Fig. 4A, and Fig. 4C is a sectional view of the portion shown in Fig. 4B;

Figs. 5A and 5B are schematic views showing an appearance of a photovoltaic element module according

to Example 3 of the present invention. Fig. 5A is a plan view of the photovoltaic element as seen from its light-receiving surface side, and Fig. 5B is a sectional view of the photovoltaic element shown in Fig. 5A, which is taken along the line 5B-5B in Fig. 5A;

Fig. 6A is a plan view of two series-connected photovoltaic elements, each of which is shown in Figs. 5A and 5B, as seen from their light-receiving surface side. Fig. 6B is an enlarged view of the series-connected portion in Fig. 6A, and Fig. 6C is a sectional view of the portion shown in Fig. 6B;

Figs. 7A and 7B are schematic views showing an appearance of a photovoltaic element module according to Example 4 of the present invention. Fig. 7A is a plan view of the photovoltaic element as seen from its light-receiving surface side, and Fig. 7B is a sectional view of the photovoltaic element shown in Fig. 7A, which is taken along the line 7B-7B in Fig. 7A;

Fig. 8A is a plan view of two series-connected photovoltaic elements, each of which is shown in Figs. 7A and 7B, as seen from their light-receiving surface side. Fig. 8B is an enlarged view of the series-connected portion in Fig. 8A, and Fig. 8C is a sectional view of the portion shown in Fig. 8B;

Figs. 9A and 9B are schematic views showing an

appearance of a photovoltaic element module according to Example 5 of the present invention. Fig. 9A is a plan view of the photovoltaic element as seen from its light-receiving surface side, and Fig. 9B is a sectional view of the photovoltaic element shown in Fig. 9A, which is taken along the line 9B-9B in Fig. 9A;

Fig. 10A is a plan view of two series-connected photovoltaic elements, each of which is shown in Figs. 9A and 9B, as seen from their light-receiving surface side. Fig. 10B is an enlarged view of the series-connected portion in Fig. 10A, and Fig. 10C is a sectional view of the portion shown in Fig. 10B;

Figs. 11A, 11B, and 11C are schematic views showing an appearance of a conventional photovoltaic element module. Fig. 11A is a plan view of the photovoltaic element as seen from its light-receiving surface side, Fig. 11B is a sectional view of the photovoltaic element shown in Fig. 11A, which is taken along the line 11B-11B in Fig. 11A, and Fig. 11C is a plan view of two series-connected photovoltaic elements as seen from their light-receiving surface side;

Fig. 12 is a sectional view schematically showing a configuration of the photovoltaic element;

Fig. 13 is a graph showing the reflective characteristics of metals;

Fig. 14 is a graph showing the relationship

between the photoabsorptivity of a medium and the welding stability;

Fig. 15 is a graph showing the welding stability of a light-absorbing medium;

5 Fig. 16 is a graph showing the relationship between the thickness of a film and the adhesive strength of the film after welding;

Fig. 17 is a schematic view showing a laser treatment method according to Example 6;

10 Figs. 18A and 18B are schematic views showing an appearance of a photovoltaic element module according to Example 7 of the present invention. Fig. 18A is a plan view of the photovoltaic element as seen from its light-receiving surface side, and Fig. 18B is a  
15 sectional view of the photovoltaic element shown in Fig. 18A, which is taken along the line 18B-18B in Fig. 18A;

Fig. 19A is a plan view of two series-connected photovoltaic elements, each of which is shown in Figs.  
20 18A and 18B, as seen from their light-receiving surface side. Fig. 19B is an enlarged view of the series-connected portion in Fig. 19A, and Fig. 19C is a sectional view of the portion shown in Fig. 19B;

Fig. 20 is a schematic view showing a method of  
25 supplying a non-contact medium;

Fig. 21 is a graph showing the relationship between the mean square surface roughness of the non-

contact medium and its welding reliability; and

Fig. 22 is a graph showing the relationship between the mean square surface roughness of the non-contact medium and its adhesion strength to a treated material.

#### DESCRIPTION OF THE PREFERRED EMBODIMENTS

Preferred embodiments of the present invention are described below with reference to the drawings.

10 (Photovoltaic element)

Fig. 12 schematically shows a sectional view of an example of a photovoltaic element used in the present invention. In this figure, numeral 701 indicates a substrate, 702 a lower electrode layer, 703 a semiconductor layer, and 704 an upper electrode layer.

The photovoltaic element shown in Fig. 12 can be applied to an amorphous silicon type solar cell which <sup>flexible</sup> <sup>has flexibility</sup> <sup>that is preferably</sup> <sup>desirably has flexibility</sup>. Such a configuration, however, can be applied to solar cells other than the amorphous type solar cells, such as a single-crystalline or polycrystalline solar cell or a solar cell using a semiconductor other than silicon or having the Schottky junction.

The substrate 701 is a member for mechanically supporting the semiconductor layer 703 in a thin solar cell of amorphous silicon type. The material for the substrate 701 may be conductive or insulating but must



be conductive when the substrate 701 also acts as an electrode. The substrate 701 must be durable enough to withstand the heating temperature for forming the semiconductor layer 703.

5       The conductive material for the substrate 701 includes metals such as Fe, Ni, Cr, Al, Mo, Au, Nb, Ta, V, Ti, Pt, and Pb; and alloys thereof, for example, a sheet metal such as brass or stainless steel; and composites thereof.

10       The electrically insulating material for the substrate 701 includes heat-resistant synthetic resins, such as polyester, polyethylene, polycarbonate, cellulose acetate, polypropylene, polyvinyl chloride, polyvinylidene chloride, polystyrene, polyamide,  
15       polyimide, and epoxy resin; and their composites with glass, carbon, boron, or metal fibers; glass; and ceramics.

*Lower electrode layer*

20       The lower electrode layer 702 is one of the electrodes for collecting electric power generated in the semiconductor layer 703 and must have a work function <sup>*in a way*</sup> such that the lower electrode layer 702 forms an ohmic contact with a semiconductor.

25       The material for the lower electrode layer 702 includes metals such as Al, Ag, Pt, Au, Ni, Ti, Mo, Fe, V, Cr, Cu, stainless steel, brass, nichrome, SnO<sub>2</sub>, In<sub>2</sub>O<sub>3</sub>, ZnO, and ITO (indium tin oxide); and alloys

thereof; and transparent conductive oxide (TCO).

The surface of the lower electrode layer 702 is <sup>preferably</sup> desirably smooth, but may be textured when it irregularly reflects light. In addition, when the substrate 701 is conductive, the lower electrode layer 702 may be omitted.

The lower electrode layer 702 may be provided by a well-known method, such as plating, deposition, or sputtering.

10 ~~Semiconductor layer~~

The semiconductor layer 703 of the photovoltaic element used in the present invention comprises a well-known semiconductor material generally used for thin film solar cells. Specifically, it is possible to use as the semiconductor layer 703, a pin-junction amorphous silicon layer, a pn-junction polycrystalline silicon layer, or a layer of a compound semiconductor such as  $\text{CuInSe}_2/\text{CdS}$ .

When the semiconductor layer 703 is an amorphous silicon layer, it can be formed by introducing a raw material gas, such as silane gas for forming a film, into a plasma CVD apparatus for generating plasma discharge. In addition, when the semiconductor layer 703 is a pn-junction polycrystalline silicon layer, it can be formed by forming a film using [a] molten silicon. When the semiconductor layer 703 consists of a compound semiconductor such as  $\text{CuInSe}_2/\text{CdS}$ , it can be formed by

the electron beam deposition method, the sputtering method, or the electrodeposition method.

#### Upper electrode layer

The upper electrode layer 704 is one of the electrodes for collecting <sup>the</sup> electromotive force generated in the semiconductor layer 703, and is paired with the lower electrode layer 702. Like the lower electrode layer 702, the upper electrode layer 704 must [have a work] function <sup>in a way</sup> such that the layer 704 forms an ohmic contact with a semiconductor. The upper electrode layer 704 is required when the semiconductor layer 703 comprises a semiconductor such as amorphous silicon having a high sheet resistance, and is not particularly required when a crystalline semiconductor is used, due to its low sheet resistance.

When the substrate 701 is opaque, the upper electrode layer 704 is necessarily located on the light incident side. In this case, the upper electrode layer 704 must transmit light, that is, must be a transparent electrode. To allow light from the sun or a <sup>white</sup> fluorescent lamp to be efficiently absorbed by the semiconductor layer 703, the light transmittance of the upper electrode layer 704 is preferably 85% or more. In addition, to allow a photoelectric current generated in the semiconductor layer 703 to efficiently flow in a direction parallel <sup>to</sup> [with] the semiconductor layer 703, the sheet resistance of the upper electrode layer 704



is preferably 100Ω or less. The material having these characteristics and preferred for the upper electrode layer includes metal oxides such as SnO<sub>2</sub>, In<sub>2</sub>O<sub>3</sub>, ZnO, CdO, CdSnO<sub>4</sub>, and ITO (In<sub>2</sub>O<sub>3</sub>+SnO<sub>2</sub>).

5 Non-contact treatment and method of producing photovoltaic element module

The non-contact treatment according to the present invention can be applied to welding or cutting of various parts including electric parts or general structures formed of either a metal material or a non-metal material by energy irradiation, to etching or patterning during a step of producing an electric-part, and to the thermal treatment of semiconductor materials.

15 In the present invention, laser welding is applied to particularly photovoltaic elements. The energy supply means used in the present invention and the medium capable of absorbing energy are described below and which are the features of the photovoltaic element module according to the present invention.

20 Energy supply means

As the energy supply means according to the present invention, light, heat or electromagnetic waves can be suitably used. Heating by irradiation of light, such as laser light, or light from a halogen lamp or a far infrared lamp can be used.

The laser used for laser welding according to the

present invention includes a solid laser such as ruby  
( $\text{Cr}^{3+}:\text{Al}_2\text{O}_3$ ), YAG ( $\text{Nd}^{3+}:\text{Y}_3\text{Al}_5\text{O}_{12}$ ), phosphate glass,  
silicate glass, YLF ( $\text{Nd}^{3+}:\text{LiYF}_4$ ), or Thailand sapphire  
( $\text{Ti}^{3+}:\text{Al}_2\text{O}_3$ ), and a gas laser such as  $\text{CO}_2$ -laser-excited  
5 or discharge-excited far infrared radiation or rare gas  
ions.

The metal material used for a system such as a  
solar cell <sup>has large</sup> [through] which a [high] current flows <sup>g</sup>  
preferably has a low resistance in order to reduce  
10 losses caused by the resistance. As shown in Fig. 13,

however, the reflectance is relatively high when the  
metal is irradiated with light having a wavelength of  
0.4  $\mu\text{m}$  or more. <sup>Thus,</sup> it has been difficult <sup>to weld metal with</sup> that laser light  
having a wavelength of 0.4  $\mu\text{m}$  or more [is] used to weld  
15 the metal]. On the other hand, the use of laser light

of less than 0.4  $\mu\text{m}$  increases the costs of ~~facilities~~ <sup>for example,</sup>  
[as in] ~~excimer lasers~~ <sup>expensive high-value</sup>. Accordingly, the use of laser  
light having a wavelength not more than 0.4  $\mu\text{m}$  has been  
limited to [high-value-added] products.

20 The present invention <sup>allows the use of</sup> [enables] laser light having a  
wavelength of 0.4  $\mu\text{m}$  or more to [be used] to weld  
metal.

Of the lasers having a wavelength of 0.4  $\mu\text{m}$  or  
more, solid lasers (the wavelength of main solid lasers  
25 is in a range of 0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$ ) <sup>are</sup> [is] more efficient  
than gas lasers and <sup>have the</sup> [has] advantages of <sup>being more compact</sup> providing <sup>and</sup>  
higher-power laser light and enabling the apparatus to

~~be compactified~~. In particular, YAG lasers have excellent characteristics such as their capabilities of transmitting laser light through optical fibers and executing welding at a position remote from a laser transmitter. They also enable the welding conditions to be changed by the selection of optical fibers and outgoing units and also enable one laser beam to be divided into about 2 to about 10 beams.

~~(Medium capable of absorbing energy)~~

10        The ~~reflective characteristic~~ <sup>reflectivity</sup> obtained when metal is irradiated with light depends on the type of metal, and is [as] shown in Fig. 13. Despite the amount of reflection depending on the wavelength, most irradiation light is reflected particularly at the long wavelength side. For example, at 0.7  $\mu\text{m}$ , which is close to the wavelength of ruby laser beams (0.69  $\mu\text{m}$ ), the reflectances of gold, silver, copper, and aluminum are 97.0%, 98.5%, 97.5%, and 89.8%, respectively. The reflectances at the YAG laser wavelength (1.06  $\mu\text{m}$ ) of gold, silver, copper, and aluminum are 98.2%, 98.9%, 98.5%, and 93.9%, respectively. Thus, it has been difficult to weld metal such as gold, silver, copper, and aluminum used for photovoltaic elements, by using the ruby or YAG laser.

25        ~~(Medium capable of absorbing at least 10% or more of laser light having wavelength of 0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$ )~~

Thus, in the present invention, a medium capable

of absorbing 10% or more of laser light is provided on a surface to be welded to reduce inappropriate welding while enabling stable laser welding. In particular, the medium preferably has an absorptivity of 10% or more at 0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$ , which is in the wavelength range of the above solid laser.

Fig. 14 shows the effects obtained by providing a medium capable of absorbing 10% or more of laser light on a surface to be welded.

Fig. 14 is a graph showing the relationship between the photoabsorptivity of the medium and welding stability obtained when a copper foil and a silver-plated copper foil (each having a thickness of 100 $\mu\text{m}$ ) having a high reflectance were selected as a metal to be irradiated with laser light and when a paint was applied uniformly to the surface of the metal as the medium, followed by the irradiation of YAG laser beams (wavelength: 1.06 $\mu\text{m}$ ) to carry out welding. A plurality of paints having different photoabsorptivities were used for evaluations. In addition, welding was carried out under conditions optimal for each reflectance (however, copper and silver-plated copper were welded under the same conditions). Furthermore, in evaluation of the welding stability, a sample after welding which exhibited a joining force of 4.0 kg or more after thermal cycle tests (200 cycles at 90°C to -40°C) and in which no holes or cracks were found in the welded

portion when observed using an optical microscope was regarded as a good product (non-defective product). Thus, all the obtained samples were evaluated based on the non-defective percentage.

5        Since copper and silver reflect 98.0% or more of laser light having a wavelength of 1.06  $\mu$ m, the welding stability of the metal is normally 40% or less. <sup>other it is</sup> they <sup>them</sup> are difficult to be subjected to laser welding. As shown in Fig. 14, however, by providing a medium  
10        capable of absorbing light on the surface of the metal, it is possible to improve the welding stability of the metal. In particular, the welding stability is 80% or more when the medium has a photoabsorptivity of 10% or more.

15        The energy (welding energy) required for welding a metal by using laser light can be represented by the following equation.

$$\text{(Welding energy)} = \text{(laser outgoing energy)} \times \text{(photoabsorptivity of metal)}$$

20        Normally, when a metal is welded using laser light, laser light having a larger energy than the welding energy must be supplied in consideration of the surface reflection of the metal. If, for example, the metal has a light reflectance of 90%, it is necessary  
25        to irradiate the metal with light having a laser outgoing energy which is 10 times as large as that required for metal welding <sup>with</sup> in the case of no reflection.



*of a metal.* Once laser light is introduced into the metal, the metal ~~is melted~~ <sup>*melts*</sup> and the ~~molten metal~~ readily absorbs laser light. Consequently, most <sup>*of the energy*</sup> supplied ~~is used for~~ <sup>*energy*</sup> ~~becomes~~ welding energy. When, however, the metal is, for example, a thin foil used for a photovoltaic element, excessive energy may increase the temperature of the irradiated portion above the melting point of the metal, resulting in holes in the metal. In the present invention, a medium capable of absorbing laser light having a wavelength of 0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$  is provided on the surface of a metal to be irradiated with laser light to restrain the reflection from the surface of the metal and allow laser light to be easily introduced into the metal. For example, in the case of executing welding that requires 5J ~~energy~~ <sup>*energy*</sup>, 50J outgoing energy is required when the reflectance of the metal is 90%, whereas it is possible to execute welding with 25J outgoing energy when the reflectance of the surface can be reduced to 80% by using a medium. That is, by providing a light-absorbing medium on the surface of metal having high surface reflection, the outgoing energy of laser light can be <sup>*considerably*</sup> ~~remarkably~~ reduced. This configuration can prevent holes from being formed in the metal.

Although the above discussion <sup>*mentions the use of*</sup> ~~uses~~ paints as the medium capable of absorbing light, the medium according to the present invention is not limited to paints <sup>*and*</sup> ~~but~~.

*appropriately*, *regardless of* the materials  
may be selected as appropriate, whether they are  
insulating or conductive <sup>or</sup> materials. The insulating  
material used for the medium according to the present  
invention, however, must be melted when heated during  
5 welding to maintain the conductivity between the metal  
members.

Specifically, the object of the present invention  
can be sufficiently achieved by coloring the surface of  
the metal member using felt pen or ink jet. The color  
10 is preferably other than white so as to provide a  
larger photoabsorption coefficient. To improve the  
welding stability, an ink application method that  
enables ink to be uniformly applied is preferably used.  
Various methods can be used, <sup>such as,</sup> for example, the hardening  
15 of a silk-screen-printed ink by using a hot air drying  
furnace.

In addition, instead of using an ink, a film  
material such as a black PET (polyethylene-  
terephthalate) film (for example, trade name: **LUMIRROR**  
20 X30, produced by Toray Industries, Inc.; and trade  
name: **MELINEX** 427, produced by ICI Japan Ltd.) may be  
stuck to the surface of the metal member, and the metal  
member may be welded together with the film by  
irradiating it with laser light from the film side.

25 After welding, the film is preferably removed, but may  
not be removed depending on the material of the film.  
*However, the film*  
*of which is composed*

When the thickness of the film is in a range of 5  $\mu$ m to

30  $\mu$ m, welding is stabilized to allow the film to be removed easily after welding.

Furthermore, when a conductive material is used as the medium, a metal material of a large photo-  
5 absorption coefficient may be selectively used.

Specifically, an iron based material, such as stainless steel, a material plated with Ni or solder, a material obtained by treating in a strong-acid solution to  
10 coated with carbon black, or a material with conductive fine particles dispersed therein may be located on the surface of the metal member, which is then welded together with the conductive material. After welding, the conductive material is preferably removed, but may  
15 not be removed depending on the material.

The metal member may be plated with Ni or solder, to use the Ni or solder as the medium capable of absorbing light.

Fig. 15 shows examples of welding stability, which  
20 were obtained when the above-mentioned media and YAG laser were used to carry out welding. The details of the media shown in Fig. 15 are as follows.

25 Felt pen: Oily Magic Ink No. 500  
Manual application  
Photoabsorptivity: 10%

Silk screen printing: Emerson & Cuming CT-5079-3A

(produced by National Starch)



& Chemical Company)

Printer

Photoabsorptivity: 60%

5 Ink jet printer:

JP-K27 (produced by Hitachi  
Manufacturing Company)

Dedicated printer

Photoabsorptivity: 25%

Black PET tape:

~~MELINEX~~  
Melinex 427 (produced by ICI  
Japan Ltd.)

10

~~LUMIRROR~~  
(~~Lumirror~~ X (produced by Toray Industries, Inc.) or  
~~LUMIRROR~~  
black-treated ~~Lumirror~~ T (produced by Toray Industries,  
Inc.)

Photoabsorptivity: 60%

15

Ni plating:

Thickness: 2  $\mu$ m to 5  $\mu$ m

Photoabsorptivity: 50%

Surface oxidation:

Electrolytic treatment

Photoabsorptivity: 20%

20

All the media provided satisfactory results, that  
is, their welding stabilities were 70% or more.

~~/~~Non-adhering medium~~/~~

The following materials are applicable as the non-  
adhering medium according to the present invention.

25

The applicable materials include paper; ~~/~~ cloth; ~~/~~  
leather; ~~/~~ thin metal foils, such as stainless steel,  
steel ~~/~~ and black alumite; polyester films, such as a  
polyethyleneterephthalate film, a polybutylene-

terephthalate film, a polyethylenenaphthalate film, a polycyclohexylenedimethyleneterephthalate film, and a polyethylenebisphenoxycarboxylate film; polyolefin films such as <sup>a</sup>polyethylene film and <sup>a</sup>polypropylene <sup>film</sup>;

5 a cellulose derivative film, such as a cellulose acetate butylate film and a cellulose acetate propionate film; vinyl resin films, such as a polyvinyl chloride film and a polyvinylidene chloride film; polymer films, such as a polystyrene film, a polyamide film, a polyimide film, a

10 polycarbonate film, a polysulfone film, a polyurethane resin film, an epoxy resin film, and a fluoride resin <sup>film</sup>, and a composite material comprising the above polymer film laminated with a thin metal foil, such as a stainless steel foil, a steel foil, or a black alumite

15 foil.

When the medium has at least the polymer film among the above materials, the polymer film is thin and strong and can be removed easily after welding because the polymer film is melted <sup>s</sup> and <sup>evaporated</sup> volatilized during energy

20 irradiation. In addition, the polymer films [is] <sup>on the market are</sup> supplied [in a] long <sup>high volume</sup> [size] so that welding can be carried out [with a high mass-productivity].

~~In addition,~~ when the medium is a magnetic tape,

The objects of the present invention are accomplished best

25 [most appropriately]. This is because this material is excellent in workability, mold-releasing capability, and high-speed treatment. The mold-releasing

capability can be further improved by attaching the magnetic surface of the magnetic tape to a material to be treated.

Furthermore, the surface of the non-adhering medium <sup>that</sup> ~~which~~ attaches to a material to be treated preferably has a surface roughness of 0.1 nm to 5,000 nm. <sup>when</sup> ~~In the case of~~ the roughness <sup>is</sup> of 5,000 nm or less, the non-adhering medium efficiently guides, for example, laser light to the material to be treated as shown <sup>on</sup> in Fig. 21. When the surface of the non-adhering medium <sup>that</sup> ~~which~~ is attached to the material to be treated has a surface roughness of 0.1 nm or more in mean square, the non-adhering medium is unlikely to stick to the treated material during laser treatment, for example, (as shown) in Fig. 22 <sup>this allows</sup> ~~thereby~~ allowing the non-adhering medium to be easily removed after laser treatment.

The methods of providing on at least <sup>a</sup> the side of the medium <sup>that</sup> ~~which~~ contacts the material to be treated by energy irradiation, recessed and protruding portions corresponding to a surface roughness of 0.1 to 5,000 nm in mean square include the use of the characteristics of the material itself <sup>in relation to</sup> ~~for~~ the medium, the surface treatment by [means of] etching or discharge, the deformation of the surface shape by [means of] pressing or scratching, the mixing of a carbon block or a color material such as pigment into the polymer film, or the

application or deposition of a selected material.

As one example of using the polyethylene-  
terephthalate film, the protrusions on the surface of  
the polyethyleneterephthalate film can be controlled by  
the selection of a polymerization medium for a raw  
material ~~polymer~~ or by adding inorganic particles to  
the film, as disclosed in Japanese Patent Publication  
No. 30-5639. More specifically, there is a method of  
adding an oxide, such as  $\text{SiO}_2$ ,  $\text{TiO}_2$ ,  $\text{CaCO}_3$ , or  $\text{Al}_2\text{O}_3$ , or an  
inorganic salt during the polymerization of the raw  
material polymer or during the melting of pellets prior  
to drawing.

In addition, the materials <sup>that are</sup> which is applied or  
deposited material onto the medium includes carbon  
black, graphite, titanium oxide, barium sulfate, zinc  
sulfide, magnesium carbonate, calcium carbonate, zinc  
oxide, calcium oxide, magnesium oxide, tungsten  
disulfide, molybdenum disulfide, boron nitride, tin  
disulfide, silicon disulfide, chromium oxide, alumina,  
silicon carbide, cerium oxide, corundum, artificial  
diamond, iron oxide, garnet, silica rock, silicon  
nitride, molybdenum carbide, boron carbide, tungsten  
carbide, titanium carbide, diatomaceous earth,  
dolomite, a lubricant such as resin powders, an  
abrasive, an anti-static agent, a dispersant, a  
pigment, <sup>also</sup> ~~and/or~~ <sup>that</sup> dyes which may be combined with the  
above materials, such as a phthalocyanine dye, an azo

can be used. <sup>for example,</sup> applicable dyes include

dye, an anthraquinone dye, an indigoid dye, a nitro  
and nitroso dyes, a quinoline dye, a methyne dye, a  
thiazole dye, a quinoneimine dye, an azine dye, an  
oxazine dye, an thiazine dye, an azoic dye, a  
5 diphenylmethane dye, a triphenylmethane dye, a xanthene  
dye, acridine dye, an oxidation dye, a sulfidization  
dye, a phthalein dye, an aminoketone dye, or an  
oxyketone dye.

Paper, ~~a~~ cloth, or a material coated with a  
10 pigment such as carbon black by using a nozzle coater  
is preferably used as a non-adhering anti-reflection  
medium because "residue" resulting from heat during  
laser treatment is unlikely to stick to the treated  
material.

15 The means for supplying the non-adhering medium is  
not particularly limited and may handle a sheet medium  
or a roll medium. However, the medium can be  
preferably attached and detached to such means and, *preferably,*  
*to facilitate* ~~desirably~~ continuously supplied ~~in consideration of~~  
20 mass production.

When a sheet-like medium is supplied, it may have  
to be replaced at the end of each treatment or a means  
may be required for offsetting a position so as to  
avoid irradiating the same position with energy. Thus,  
25 the medium is preferably supplied from the form of a  
roll and is desirably wound up after treatment. When  
the medium is shaped like a roll, it can be



continuously supplied by using a simple delivery and winding mechanisms, thereby enabling mass production.

Material to be treated

The material to be treated may be selected from various metal materials or non-metal materials, and is not limited. The present invention, however, is particularly effective for a material having a low absorption characteristic with respect to an used energy. Specifically, the present invention is

effective for a high-reflection material having <sup>reflecting</sup> ~~reflectance of 40% or more of <sup>the</sup> used energy~~ or <sup>transmitting at least</sup> ~~transmittance of 40% or more of <sup>the</sup> used energy~~ for treatment

~~As the specific metal material to be treated, it is possible to use a metal such as Fe, Ni, Cr, Al, Mo, Au,~~

Nb, Ta, V, Ti, Pt, Pb, Ag, or Cu, or an alloy thereof, for example, stainless steel, brass, or nichrome. In particular, as a metal material used for an electrode <sup>in</sup> ~~for~~ an electric part through which a current flows, a

material <sup>such as gold, silver, copper, or aluminum</sup> ~~is~~ <sup>because they have</sup> ~~preferably used that has a low resistance, to reduce~~ <sup>thereby reducing</sup>

<sup>due to</sup> resistance ~~losses~~. Laser light, however, is noticeably reflected from the above metals as described above

(Fig. 13). <sup>It</sup> ~~It~~ has been difficult to directly irradiate these metals with laser light having a wavelength of

0.4  $\mu\text{m}$  or more. Laser light having a wavelength <sup>of</sup> less than 0.4  $\mu\text{m}$  requires <sup>expensive equipment, such as</sup> ~~expensive facilities as in excimer~~ lasers, and is unlikely to supply a high energy ~~amount of~~

<sup>sufficiently</sup>

required for welding or cutting. Consequently, the application of such laser light has been limited.

In addition, as the non-metal material to be treated, it is possible to use a synthetic resin such as polyester, polyethylene, polycarbonate, cellulose acetate, polypropylene, polyvinyl chloride, polyvinylidene chloride, polystyrene, polyamide, polyimide, an epoxy resin, or a fluoro-resin <sup>or</sup> glass fibers, carbon fibers, or boron fibers, and glass or ceramics *may also be used*

The ~~Material~~ to be removed or the semiconductor material ~~to be~~ thermally treated by laser light during etching or patterning in the step of producing an electric part includes <sup>single-crystalline</sup> silicon, polycrystalline silicon, amorphous silicon, <sup>a</sup> ~~compound~~ *-containing compound,* silicon, such as  $\text{CuInSe}_2$ ,  $\text{CdS}$ , and  $\text{SnO}_2$ ,  $\text{In}_2\text{O}_3$ ,  $\text{ZnO}$ , or ITO (indium tin oxide).

The connection method according to the present invention has been accomplished by the inventors conducting experiments and detailed investigations in order to ~~realize~~ <sup>devise</sup> a method ~~which~~ <sup>that</sup> is reliable and can be easily automated ~~in production of~~ <sup>to produce</sup> a photovoltaic element module by electrically connecting at least two photovoltaic elements in series or in parallel. This method has the following effects.

(1) Since operations are completed ~~for a time~~ <sup>faster</sup> shorter than ~~that~~ <sup>by</sup> the conventional techniques and a

welding point has <sup>the</sup> a smallest area, the present invention has <sup>fewer</sup> ~~few~~ portions adversely affected by heat. Thus, <sup>the present invention allows to achieve</sup> ~~it can obtain~~ almost all the specific

characteristics of the semiconductor. ~~This effect can~~

5 <sup>A improvement may be accomplished</sup> ~~be further improved~~ by separating a portion where welding is carried out by laser from effective areas via etching lines.

(2) In connecting photovoltaic elements each comprising a semiconductor element provided on the metal substrate, the metal substrate separated from the effective areas via etching lines can be directly used as an output terminal electrode, thereby omitting the step of forming a terminal to reduce the non-electric power-generation area. This also applies to conductive substrates other than metal substrates.

(3) In electrically connecting adjacent photovoltaic elements to each other, a metal member is provided on the electrode portion of the semiconductor element and the metal members of the photovoltaic elements <sup>are</sup> ~~were~~ electrically connected to each other by [using] laser welding. Therefore, the semiconductor is ~~not~~ almost affected by the adverse effect of heat, thereby avoiding restrictions on the <sup>formed</sup> connection ~~form~~ to enable arbitrary designs.

25 (4) A conductive adhesive can be used to join the semiconductor layer and collecting electrode of the photovoltaic element together and to join together the



collecting electrode of the photovoltaic element and  
the metal member provided on the electrode portion <sup>for simplification</sup>  
~~in order to simplify the steps~~ In the conventional  
techniques using solder, heating for melting and fixing  
5 solder causes the conductive adhesive to ~~be degraded~~ <sup>to</sup>  
~~reduce~~ <sup>reducing</sup> the yield. The present invention, however,  
solves this problem <sup>allowing</sup> to ~~enable~~ the conductive adhesive  
<sup>to produce</sup> to be used ~~in the steps of producing~~ a photovoltaic  
element module.

10 (5) When the metal members are welded together by  
laser light, the metal material has ~~a reflection~~ <sup>reflective</sup>  
characteristics <sup>these</sup> such as ~~that~~ shown in Fig. 13, and  
<sup>must be</sup> Therefore, laser light ~~is required to have~~ a higher  
<sup>due to</sup> energy ~~by the~~ surface reflection losses of the metal  
15 ~~than that~~ <sup>is</sup> actually required for welding. However, once  
laser light is introduced into the metal, the metal ~~is~~  
melted <sup>s</sup> and readily absorbs laser light, thereby  
changing most of the supplied energy to welding energy.  
In this case, when the metal member is, for example, a  
20 thin foil used for a thin photovoltaic element, an  
excessive amount of energy <sup>raises</sup> ~~increases~~ the temperature of  
the portion irradiated with laser light, above the  
boiling point of the metal, <sup>causing</sup> ~~to cause~~ holes to be formed  
in the metal member. In the present invention, a  
25 medium capable of absorbing 10% or more of laser light  
having a wavelength of 0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$  is provided on  
the surface of the metal member to restrain the

FOOTNOTES

reflection from the surface of the metal member in order to allow laser light to be easily introduced into the metal member. This configuration can reduce the outgoing energy of the laser to simplify the welding of metal with <sup>a</sup>high surface <sup>reflectance</sup> reflection, and stabilizes the welding strength, thereby providing a reliable photovoltaic element module. In addition, the outgoing energy can be restricted to increase the lifetime of an expensive outgoing lamp, thereby reducing running costs.

(6) An excellent solar cell can be provided by forming a metal member consisting of at least one of gold, silver, copper, stainless steel, and aluminum as a main component. The metal member from which electric power generated by the photovoltaic element is externally obtained <sup>must comprise</sup> ~~is required to be~~ a conductive material that minimizes output losses and <sup>has</sup> ~~have~~ a high weather resistance, for example, <sup>highly</sup> ~~a~~ long-term stability. A <sup>highly</sup> ~~very~~ conductive photovoltaic element module <sup>having</sup> ~~with~~ few resistance losses can be provided by using ~~one of~~ gold, silver, copper, stainless steel, <sup>or</sup> ~~and~~ aluminum.

In particular, stainless steel can be used to provide a relatively inexpensive photovoltaic element module ~~that has a rust and a weather-resistance~~.

(7) The method of providing ~~on the surface of the metal member irradiated with laser light~~ a medium capable of absorbing 10% or more of laser light having

then employing

on the surface of the metal member can

a wavelength of 0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$ ) includes ~~a method of~~  
using as a medium a part of the metal member used for  
the photovoltaic element, ~~and a method of~~  
supplementarily supplying a medium during the  
5 production step, ~~one of which can be selectively used~~  
~~The method of using~~ <sup>wherein</sup> a part of the metal member <sup>is used</sup> as the  
medium includes ~~a method of~~ treating the metal member  
in a strong-acid solution to oxidize or etch its  
surface, ~~a method of~~ plating the surface of the metal  
10 member, and ~~a method of~~ coating the surface of the  
metal member with carbon black. In addition, the  
method of supplementarily supplying the medium during  
the production step includes ~~a method of~~ closely  
contacting a material of a low surface reflectance <sup>with</sup>  
15 the surface of the metal member and irradiating the  
metal member with laser light, from the side of the  
material ~~of a low surface reflectance~~ to weld the metal  
member together with the material <sup>that has</sup> ~~of a low surface~~  
reflectance. After welding, the material is preferably  
20 removed, but may not be removed depending on the  
material.

(8) When the medium capable of absorbing light is  
a color ink provided on the surface of the metal  
member, ~~it can be provided most simply~~. <sup>the process of applying the ink is very simple</sup> The method of

25 ~~providing the color ink includes a method of applying~~  
~~the ink by using a felt pen, a method of~~ <sup>jetting</sup> jetting the  
ink, ~~and a method of printing the ink by using silk~~  
<sup>can be applied by either</sup>

*a highly reflective*

screen printing, ~~one of which can be selectively used.~~  
Even when metal is used ~~that is easy to reflect laser~~  
~~light~~, a color ink can be provided on the surface of  
the metal to allow laser light to be easily introduced  
5 into the metal, thereby providing a stable welding  
strength to form a very reliable photovoltaic element  
module.

(9) The most stable welding strength can be  
obtained when the medium capable of absorbing laser  
10 light, which is provided on the surface of the metal  
member, is a film having a thickness of 5  $\mu\text{m}$  ~~and~~ <sup>to</sup> 30  $\mu\text{m}$ .  
Based on the film characteristics, the film material is  
selected [so as] to match the wavelength of laser light  
used, and is advantageous in controlling quality, such  
15 as thickness. In addition, when the metal member is  
irradiated with laser light from the film side to weld  
the metal member with the film, the film can be easily  
peeled off after welding when the thickness of the film  
is from 5  $\mu\text{m}$  to 30  $\mu\text{m}$ .

20 (10) When the medium capable of absorbing laser  
light, which is provided on the surface of the metal  
member, consists of at least Fe, Ni, or solder, the  
welding strength can be stabilized, and the number of  
operations can also be reduced by [previously <sup>plating</sup> providing]  
25 Fe, Ni, or solder on the surface of the metal member  
using plating. The material for the metal member from  
which electric power generated by the photovoltaic

*having*  
*Characteristics*  
element is externally obtained must be conductive to  
minimize output losses <sup>0</sup> and must <sup>also be</sup> have a weather  
resistance, such as long-term stability <sup>0</sup> and therefore, <sup>a</sup>  
material plated with Fe, Ni, or solder is preferably  
5 used when the metal member comprises, for example,  
copper.

The non-contact treatment of the present invention  
is an improved non-contact treatment using, for  
example, laser or halogen light to cut or weld a high-  
10 reflection material, such as gold, silver, copper, or  
aluminum that is often used for electric parts, such as  
photovoltaic elements, ~~and has been obtained by the~~  
~~inventors conducting experiments to obtaining knowledge~~  
~~and executing further investigations.~~ In addition to  
15 the effects described in the above (1) to (6), this  
method has the following effects.

(11) The present invention provides a non-contact  
treatment method <sup>whereby</sup> ~~of carrying out treatment by supplying~~  
<sup>is supplied</sup> energy from an energy supply means, comprising placing  
20 on a material to be treated a non-adhering medium  
capable of absorbing energy and irradiating the non-  
adhering medium with energy. This method can achieve  
stable non-contact treatment because the physical  
characteristics of the placed medium determines the  
25 reflectance, <sup>can</sup> and enables high-speed treatment, because  
the non-adhering anti-reflection material can be  
removed after the non-contact treatment.

(12) When the surface of the non-adhering medium that closely contacts the material to be treated has a surface roughness of 0.1 nm to 5,000 nm in mean square, more stable welding is possible and the non-adhering anti-reflection material can be removed easily. Beyond 5,000 nm, stable treatment is impossible because the medium does not closely contact the material, whereby energy is not efficiently introduced to the inside of the material to be treated. In addition, below 0.1 nm the non-adhering medium ~~closely contacts the material to be treated~~ but significantly sticks to the material during energy irradiation, whereby the medium is not easily removed after the treatment.

(13) When the non-adhering medium has at least a polymer film, that is, when it is, for example, a polyethyleneterephthalate film mixed with carbon black, a polyethylenenaphthalate film with carbon black coated or deposited on its surface, or a material with a stainless steel foil laminated thereon, it can be removed more easily after energy irradiation because the above material is very strong and thin and because the polymer film is dissolved and volatilized during energy irradiation. In addition, polymer films are supplied in a long size enough to easily enable mass production.

(14) The effect of the present invention can be most effectively <sup>observed</sup> exhibited when the non-adhering medium



is a magnetic tape. The magnetic tape is excellent in stable workability, mold-releasing capability, and high-speed treatment. The mold-releasing capability can be improved by closely contacting the surface of the magnetic tape with the material to be treated.

(15) An object of the present treatment method is to efficiently guide energy to the material to be treated, and the particularly suitable energy is light, heat, or electromagnetic waves.

(16) The anti-reflection material (non-adhering medium) is irradiated with energy while the non-adhering medium is holding the material to be treated, whereby the medium and the material <sup>are in close</sup> ~~closely~~ contact with each other <sup>stably</sup> ~~stably~~ to <sup>stabilize</sup> ~~make~~ treatment <sup>stable</sup> ~~stable~~.

(17) Since the non-adhering medium is removed by energy irradiation and/or after <sup>the</sup> non-contact treatment, <sup>the</sup> ~~no~~ non-adhering medium <sup>does not</sup> remains in the treated part after the non-contact treatment, thereby preventing <sup>problems</sup> ~~inconvenience in appearance and defects from occurring~~ <sup>in post-process</sup> ~~in post-process~~.

(18) When the non-adhering medium is supplied ~~from~~ <sup>which is</sup> in the form of a roll, ~~of the medium and then~~ is wound up after energy irradiation, it can be continuously supplied to enable mass production and to increase the treatment speed.

(19) An object of the present non-contact treatment <sup>invention is to achieve a stable,</sup> ~~is to achieve stable treatment, therefore it~~ <sup>which is</sup> ~~therefore it~~.

is particularly suitable for welding or cutting.

(20) When the material to be treated is an electrode ~~for an electric part~~, it can be joined stably and reliably. In particular, when the material to be treated is an electrode for a photovoltaic element, the non-adhering and anti-reflection medium does not remain on the electrode portion, <sup>improving</sup> ~~to improve~~ the appearance while avoiding the need to account for the compatibility with a package material.

10 Examples of the present invention are described below.

Example 1

15 Figs. 1A to 2C are schematic views showing the appearance of a photovoltaic element module according to Example 1 of the present invention. Fig. 1A is a plan view of a photovoltaic element as seen from its light-receiving surface, and Fig. 1B is a sectional view of the photovoltaic element shown in Fig. 1A, which is taken along line 1B-1B in Fig. 1A. In addition, Fig. 2A is a plan view of two photovoltaic elements connected in series as seen from their light-receiving surface, Fig. 2B is an enlarged view of the series-connected portion in Fig. 2A, and Fig. 2C is a sectional view of Fig. 2B.

25 In Fig. 1A, reference numeral 100 indicates a 300 mm x 280 mm photovoltaic element comprising a substrate 102, a lower electrode layer 103, a semiconductor layer

104 consisting of amorphous silicon and having a photovoltaic function, and an upper electrode layer 105.

In this example, the substrate 102 for supporting the entire photovoltaic element comprises a stainless steel plate having a thickness of 150 $\mu$ m. An Al layer of about 2,000 Å in thickness and a ZnO layer of about 13,000 Å in thickness were sequentially formed on the substrate 102 as the lower electrode layer 103 by using the sputtering method. In addition, the semiconductor layer 104 was formed by sequentially stacking an n-, i-, p-, n-, i-, and p-type semiconductor layers this order from the substrate side by using the plasma CVD method. The thickness of these layers was about 150 Å, 4,000 Å, 100 Å, 100 Å, 800 Å, and 100 Å, respectively. In addition, the upper electrode layer 105 was a transparent electrode consisting of a thin indium oxide film of about 700 Å thickness, and was formed by depositing In in an O<sub>2</sub> atmosphere using the resistance heating method. Furthermore, to prevent an effective light-receiving area from being affected by the adverse effect of a short circuit between the substrate and the transparent electrode that may occur when the outer circumference of the photovoltaic element is cut, etching paste containing FeCl<sub>3</sub> or AlCl<sub>3</sub> was coated on a part of the upper electrode layer 105 by using screen printing, and was heated and washed to linearly remove

the part of the upper electrode layer 105 in order to form an etching line 101.

Subsequently, a copper foil strip <sup>e</sup> of 10 mm <sup>long</sup> in width, 285 mm in length, and 100  $\mu$ m <sup>in thickness</sup> was formed near one side (280 mm long) of the back surface (on the substrate 102 side) of the photovoltaic element as a rear-surface-side conductive foil 109, using the method described in Japanese Patent Application Laid-Open No. 8-139349. One side of the copper foil strip protruded out from the photovoltaic element 100, as shown in Fig. 1A.

Subsequently, an insulating adhesive tape 108 comprising <sup>2</sup> polyimide as a base and having a width of 10 mm, a length of 280 mm, and a thickness of 50  $\mu$ m was applied to one side of the front surface (upper electrode layer 105 side) of the photovoltaic element <sup>no</sup> such that the tape 108 was opposed to the back-surface-side conductive foil 109.

Subsequently, a carbon-coating wire comprising a copper wire <sup>1</sup> of 100  $\mu$ m <sup>in</sup> diameter <sup>and</sup> coated with <sup>a</sup> carbon paste was formed on the front side surface of the photovoltaic element as a collecting electrode 106. In this case, the carbon-coating wires were continuously formed on the upper electrode layer 105 and the insulating adhesive tape 108 at a pitch of 14 mm in such a manner <sup>↑</sup> that the wires crossed the insulating tape.

Furthermore, a front-surface-side conductive foil  
107 that <sup>is also important as a</sup> ~~was~~ a further collecting electrode different  
from the collecting electrode 106, <sup>first</sup> was formed on the  
insulating adhesive tape 108. The front-surface-side  
5 conductive foil 107 was formed by <sup>that was</sup> placing a copper foil  
strip of 20 mm <sup>in</sup> width, 285 mm <sup>long</sup> in length, and 100  $\mu$ m  
in thickness on the insulating adhesive tape 108, with  
~~interposition~~ of a part of the collecting electrode 106  
<sup>interposed</sup> therebetween, and <sup>then</sup> heating, <sup>and</sup> pressurizing <sup>fixing</sup> the  
10 strip at 200°C and 3 kg/cm<sup>2</sup> for 180 seconds. One side  
of the copper foil strip <sup>is</sup> protruded out from the  
photovoltaic element 100 at a side opposite to the  
back-surface-side conductive foil 109, as shown in Fig.  
1A.

15 To use for electric power generation the  
photovoltaic element produced in this manner, a  
plurality of photovoltaic elements were electrically  
connected in series to produce a photovoltaic element  
module. The connection method is described in Figs. 2A  
20 to 2C.

As shown in Figs. 2A to 2C, two adjacent  
photovoltaic elements were arranged in such a way, that  
a part of the front-surface-side conductive foil 107 of  
a photovoltaic element 1 overlapped a part of the back-  
25 surface-side conductive foil 109 of a photovoltaic  
element 2 over a distance of 3 mm.

Then, the overlapping portion between the front-

surface-side conductive foil 107 of the photovoltaic element 1, the back-surface-side conductive foil 109 of the photovoltaic element 2 was irradiated with laser light to be welded, thereby mechanically and electrically <sup>connecting</sup> ~~connect~~ the two elements together.

Reference numeral 110 is a welding point. The laser for providing a <sup>sufficiently</sup> high power ~~enough~~ to weld a metal preferably has a wavelength of 0.4  $\mu\text{m}$  and more ~~and is particularly preferably~~ <sup>is particularly preferable</sup> A solid laser having a wavelength of 0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$ . ~~The applicable lasers~~ includes a YAG laser, a phosphate glass laser, a silicate glass laser, and a  $\text{CO}_2$  laser. <sup>In</sup> This example, ~~used~~ a YAG laser (wavelength: 1.06  $\mu\text{m}$ ) was used to carry out <sup>the</sup> welding under the following conditions:

outgoing energy: 15.0J; pulse width: 5.0 ms; welding point diameter: 0.5 mm; number of welding points: 6.

Subsequently, the electric resistance of the laser welded portion was measured at 0.013  $\Omega$ . With respect to the performance of the photovoltaic element 100, the effective area was 809.0  $\text{cm}^2$ , the generated current density was 5.38 A, the generated current was 5.38 A, the generated voltage was 1.2 V, and the generated electric power was 6.45 W. <sup>Therefore</sup> the resistance loss of the laser welded portion was 0.9 mW. This corresponds to only 0.015% of the electric power generated by the photovoltaic element 100.

In addition, the tensile strength of the laser



welded portion was measured to be in a range of 8 kg to 15 kg.

In this example, with respect to the time required for laser welding, 2.0 seconds were required for feed-in and positioning of the photovoltaic elements 1 and 2, 3.5 seconds were required for welding (including the movement of the laser beam outgoing tip), and 1.0 second was required for feed-out of the elements. Thus, the connection of the two photovoltaic elements was completed in 6.5 seconds.

That is, this example can provide a reliable series-connected photovoltaic element module that is produced at a speed higher than that of the conventional examples, <sup>as well as</sup> a method of producing it.

Example 2

Figs. 3A to 4C are schematic views showing the appearance of a photovoltaic element module according to Example 2 of the present invention. Fig. 3A is a plan view of a photovoltaic element as seen from its light-receiving surface, and Fig. 3B is a sectional view of the photovoltaic element shown in Fig. 3A, which is taken along the line 3B-3B in Fig. 3A. In addition, Fig. 4A is a plan view of two photovoltaic elements connected in series as seen from their light-receiving surface, Fig. 4B is an enlarged view of the series-connected portion in Fig. 4A, and Fig. 4C is a sectional view of Fig. 4B.

In this example, a material was previously plated with Ni on a portion to be irradiated with laser light. The Ni plating was used as a medium capable of absorbing light.

5 In Fig. 3A, reference numeral 200 indicates a 300 mm x 280 mm photovoltaic element comprising a substrate 202, a lower electrode layer 203, a semiconductor layer 204 consisting of amorphous silicon and having a photovoltaic function, and an upper electrode layer 10 205. Reference numeral 201 designates an etching line, 206 a collecting electrode, 207 a front-surface-side conductive foil that is a further collecting electrode different from the collecting electrode 206, 208 an insulating adhesive tape, and 209 a back-surface-side 15 conductive foil. These components were formed of the same materials as in Example 1 by using the same method as in Example 1. The front-surface-side conductive foil 207 and the rear-surface-side conductive foil 209 were formed [so as] not to protrude out from the 20 photovoltaic element 200.

A plurality of the above photovoltaic elements were electrically connected in series. The connection method is described with reference to Figs. 4A to 4C.

25 In this example, <sup>was employed</sup> used a connection member 211 for connections. First, the metal member 211, which <sup>was</sup> ~~was~~ the connection member, was arranged [in such a way as] to be <sup>in contact with</sup> the photovoltaic elements 1 and 2, as shown in

Fig. 4C. Then, the metal member was irradiated with YAG laser light (indicated by the arrows in Fig. 4C) in the same manner as in Example 1 ~~except for the use of~~ <sup>put</sup> 6.0J ~~outgoing~~ <sup>was</sup> energy. Reference numeral 210 denotes a welding point. The metal member 211 comprised ~~an Ni-~~ <sup>a nickel</sup> plated copper material (width: 10 mm; length: 275 mm; thickness: 100  $\mu$ m) <sup>consisting of an inexpensive and</sup> ~~conductive copper material plated with~~ <sup>a 2  $\mu$ m thick nickel containing</sup> ~~Ni material~~ <sup>that</sup> ~~having a thickness of 2  $\mu$ m which~~ absorbs about 50% of YAG laser light having a wavelength of 1.06  $\mu$ m. Since ~~Ni~~ <sup>nickel</sup> absorbs YAG laser light much better than copper (that is, ~~Ni~~ <sup>nickel</sup> has fewer losses caused by reflection from the surface of the metal), the ~~outgoing~~ <sup>put</sup> energy of the YAG laser could be ~~restrained~~ <sup>reduced</sup> <sup>on</sup>. This example, ~~used~~ <sup>was</sup> 6.0J ~~outgoing~~ <sup>put</sup> energy from the YAG laser, but good welding results <sup>min</sup> could be obtained <sup>still</sup> ~~under this condition as in~~ Example 1.

Although, in this example, the medium capable of absorbing light was provided by plating the metal material (copper material) with ~~Ni~~ <sup>nickel</sup>, the effects shown in Fig. 15 as described above could be obtained <sup>using</sup> ~~when a~~ metal member coated with carbon black was ~~used~~.

That is, this example can provide a reliable series-connected photovoltaic element module that ~~requires lower~~ <sup>low</sup> costs than Example 1 and that operates faster than the conventional examples, <sup>as well as</sup> and its producing method.

9  
(Example 3)

Figs. 5A and 5B and 6A to 6C are schematic views showing the appearance of a photovoltaic element module according to Example 3 of the present invention. Fig.

5 5A is a plan view of a photovoltaic element as seen from its light-receiving surface, and Fig. 5B is a sectional view of the photovoltaic element shown in Fig. 5A, which is taken along the line 5B-5B in Fig. 5A. In addition, Fig. 6A is a plan view of two  
10 photovoltaic elements connected in series as seen from their light-receiving surface, Fig. 6B is an enlarged view of the series-connected portion in Fig. 6A, and Fig. 6C is a sectional view of Fig. 6B.

In this example, a portion to be irradiated with  
15 laser light was previously coated with a color ink as a medium capable of absorbing light.

In Fig. 5A, reference numeral 300 indicates a 300 mm x 280 mm photovoltaic element comprising a substrate 302, a lower electrode layer 303, a semiconductor layer  
20 304 consisting of amorphous silicon and having a photovoltaic function, and an upper electrode layer 305. Reference numeral 301 designates an etching line, 306 a collecting electrode, 307 a front-surface-side conductive foil that is a further collecting electrode  
25 different from the collecting electrode 306, 308 an insulating adhesive tape, and 309 a back-surface-side conductive foil. These components were formed of the

same materials as in Example 1 by using the same method as in Example 1.

A plurality of the above photovoltaic elements were electrically connected in series. The connection method is described with reference to Figs. 6A to 6C.

As shown in Figs. 6A to 6C, two adjacent photovoltaic elements were arranged in such a way that a part of the front-surface-side conductive foil 307 of the photovoltaic element 1 and a part of the back-surface-side conductive foil 309 of the photovoltaic element 2 overlapped each other over a distance of 3 mm.

Then, a blue felt pen (Oily Magic ink No. 500) was used to coat a color ink 313 (having an absorptivity of 30% at a wavelength of 1.06  $\mu\text{m}$ ) as a medium capable of absorbing light on the overlapping portion of the front-surface-side conductive foil 307 of the photovoltaic element 1. Welding points 310 in the area coated with the color ink 313 were irradiated with a YAG laser under the same conditions as in Example 2 to mechanically and electrically connect the two conductive foils to each other. For example, a solid laser having a wavelength of 0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$  may be used instead of the YAG laser.

This example produced good results similar to those in Example 2.

Similar results were obtained by using a color ink

having an absorptivity of 10% (a sky blue felt pen) <sup>instead</sup> ~~in~~  
~~place~~ of the color ink 313 ~~used in this example~~. In  
addition, similar results were obtained by using ink  
jet or silk screen printing instead of a felt pen.

5

(Example 4)

10 Figs. 7A and 7B and 8A to 8C are schematic views  
showing the appearance of a photovoltaic element module  
according to Example 4 of the present invention. Fig.  
7A is a plan view of a photovoltaic element as seen  
from its light-receiving surface, and Fig. 7B is a  
sectional view of the photovoltaic element shown in  
Fig. 7A, which is taken along the line 7B-7B in Fig.  
7A. In addition, Fig. 8A is a top view of two  
15 photovoltaic elements connected in parallel as seen  
from their light-receiving surface, Fig. 8B is an  
enlarged view of the series-connected portion in Fig.  
8A, and Fig. 8C is a sectional view of Fig. 8B.

20 In this example, metal substrates were connected  
in parallel by ~~using~~ laser welding. In Fig. 7A,  
reference numeral 400 indicates a 300 mm x 280 mm  
photovoltaic element comprising a substrate 402, a  
lower electrode layer 403, a semiconductor layer 404  
consisting of amorphous silicon and having a  
photovoltaic function, and an upper electrode layer  
25 405. Reference numeral 401 designates an etching line,  
406 a collecting electrode, 407 a front-surface-side  
conductive foil that is a further collecting electrode



different from the collecting electrode 406, 408 is an insulating adhesive tape. These components were formed of the same materials as in Example 1 by using the same method as in Example 1. Since, however, the metal substrate 402 was used as a back-surface-side terminal, the back-surface-side conductive foil was not particularly provided. In addition, the front-surface-side conductive foil 407 was formed [so as] not protrude out from the photovoltaic element 400.

10 A plurality of photovoltaic elements were electrically connected in parallel. The connection method is described with reference to Figs. 8A to 8C.

As shown in Figs. 8A to 8C, two adjacent photovoltaic elements <sup>②</sup> were arranged in such a way that the substrate 400 of the photovoltaic element 1 and the substrate 400 of the photovoltaic element 2 <sup>were in</sup> ~~close~~ contact ~~each other~~. The closely contacting portion between the two substrates was irradiated with YAG laser light to weld and connect them to each other.

20 Although this example used the YAG laser, one of the other lasers described above may be <sup>employed</sup> used. Since this example used as the substrate 400 stainless steel mainly consisting of Fe (having an absorptivity of about 30% at a wavelength of 1.06  $\mu$ m), stable welding could be achieved <sup>while applying</sup> ~~with a~~ low energy.

25 Subsequently, a metal member 411, <sup>which also functioned as</sup> ~~that was a~~ connection member, was [arranged in such a way as] to ~~be placed~~

contact the front-surface-side conductive foils 407 of the photovoltaic elements 1 and 2, and the metal member 411 was irradiated with YAG laser light to weld the elements together in order to connect them in parallel.

5 Reference numeral 410 indicates a welding point. The metal member 411 was similar to the metal member 211 and the welding conditions were similar to these in Example 2.

10 The present invention enables both the front and back sides to be stably welded <sup>at</sup> ~~with~~ low costs, and provides a parallel-connected photovoltaic element module having <sup>an</sup> ~~an~~ excellent connection stability, <sup>as well as</sup> ~~and~~ a method of producing it.

Example 5

15 Figs. 9A to 10C are schematic views showing the appearance of a photovoltaic element module according to Example 5 of the present invention. Fig. 9A is a plan view of a photovoltaic element as seen from its light-receiving surface, and Fig. 9B is a sectional  
20 view of the photovoltaic element shown in Fig. 9A, which is taken along the line 9B-9B in Fig. 9A. In addition, Fig. 10A is a plan view of two photovoltaic elements connected in series as seen from their light-receiving surface, Fig. 10B is an enlarged view of the  
25 series-connected portion in Fig. 10A, and Fig. 10C is a sectional view of Fig. 10B.

In this example, a film was previously arranged on

a portion to be irradiated with laser light, as a medium capable of absorbing light.

In Fig. 9A, reference numeral 500 indicates a 300 mm x 280 mm photovoltaic element comprising a substrate 502, a lower electrode layer 503, a semiconductor layer 504 consisting of amorphous silicon and having a photovoltaic function, and an upper electrode layer 505. Reference numeral 501 designates an etching line, 506 a collecting electrode, 507 a front-surface-side conductive foil that is a further collecting electrode different from the collecting electrode 506, 508 an insulating adhesive tape, and 509 a back-surface-side conductive foil. These components were formed of the same materials as in Example 1 by using the same method as in Example 1. The back-surface-side conductive foil 509 was formed ~~so as~~ not to protrude out from the photovoltaic element 500. The front-surface-side foil 507 was 10 mm <sup>e</sup> in width, 285 mm <sup>long</sup> in length, and 100 $\mu$ m <sup>e</sup> in thickness, and one side of the foil 507 extended outward from the photovoltaic element 500.

A plurality of photovoltaic elements were electrically connected in series. The connection method is described with reference to Figs. 10A to 10C.

As shown in Figs. 10A to 10C, two adjacent photovoltaic elements were arranged in such a way that a part of the front-surface-side conductive foil 507 of the photovoltaic element 1 and a part of the back-

surface-side conductive foil 509 of the photovoltaic element 2 overlapped ~~each other~~ over a distance of 3 mm. In this case, the interval between the photovoltaic elements 1 and 2 was 2 mm.

5        A film 513 was arranged as a medium capable of absorbing light on the overlapping portion between the front-surface-side conductive foil 507 of the photovoltaic element 1 and the back-surface-side conductive foil 509 of the photovoltaic element 2.

10       This example used a black PET (polyethylene-terephthalate) tape (~~Melinex~~ <sup>MELINEX</sup> 427, produced by ICI Japan Ltd.; absorptivity at a wavelength of 1.06  $\mu\text{m}$ : 65%; thickness <sup>(20</sup>  $\mu\text{m}$ ; width: 13 mm) was used as the film 513. Welding points (not shown in the drawings) on the surface of the film 513 were irradiated with YAG laser light as shown by the arrows in Fig. 10C to mechanically and electrically connect the two conductive foils to each other. For example, a solid laser having a wavelength of 0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$  may be used instead of the YAG laser.

15       used instead of the YAG laser.

20       used instead of the YAG laser.

This example provided good results, similar to <sup>those obtained</sup> in Example 2.

When a film is used as the medium, as in this example, a film having a thickness of 5  $\mu\text{m}$  to 30  $\mu\text{m}$  is preferable because <sup>this</sup> the film can be easily removed after welding. When the thickness of the film is <sup>less</sup> smaller than 5  $\mu\text{m}$ , the film is likely to be torn off while

25       preferable because the film can be easily removed after welding. When the thickness of the film is smaller than 5  $\mu\text{m}$ , the film is likely to be torn off while

being peeled off. In addition, when the thickness of the film is <sup>greater</sup> ~~larger~~ than 30  $\mu$ m, the adhesion strength of the film becomes excessively high <sup>as</sup> shown in Fig. 16, thereby requiring a strong force <sup>to</sup> ~~for~~ <sup>off</sup> ~~peeling~~ the film

5 off. As a result, the welded metal member may be deformed or the film may be torn off. In Fig. 16, symbol (1) designates <sup>LUMIRROR</sup> ~~Lumirror~~ X (produced by Toray Industries, Inc.), symbol (2) denotes <sup>MELINEX</sup> ~~Melinex~~ 427 (produced by ICI Japan Ltd.), or symbol (3) indicates 10 OPP silicon (produced by Panac Co., Ltd.). Fig. 16 shows the results obtained when used the films (1), (2) and (3). Such an increase in adhesion strength is caused by the adhesion of the film base material (medium) melted by laser light of a constant diameter 15 to the metal member. This <sup>does not present a</sup> ~~characteristic has no~~ problem when the film base material is so thin that only a small amount of <sup>the</sup> ~~base~~ material is melted, <sup>However,</sup> ~~whereas~~ when the thickness of the film base material is <sup>greater</sup> ~~beyond~~ a <sup>certain</sup> ~~constant~~ value, <sup>and</sup> the melted amount of <sup>the</sup> ~~base~~ material 20 and the adhesion strength exhibit a positive correlation, ~~thereby resulting in a problem.~~

The present invention is not limited to the above examples.

Example 6

25 According to this example, an aluminum sheet that constituted an electrode for an electric part was cut. Fig. 17 is a schematic view showing a laser treatment

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a problem arises

method according to Example 6 of the present invention.

In Fig. 17, reference numeral 800 indicates the irradiation of CO<sub>2</sub> laser excited infrared light, and reference numeral 801 indicates a non-adhering medium

5. consisting of black polyethyleneterephthalate film 10mm ~~in thickness~~ <sup>wide</sup>, 13 cm ~~in length~~ <sup>long</sup>, and 0.3 mm ~~in thickness~~ <sup>thick</sup>.

Although this example used as the non-adhering medium 801

~~801~~ a <sup>MELINEX</sup> Melinex 427 film produced by ICI Japan Ltd., the experiments conducted by the inventors confirmed that

- 10 performance similar to that of this example could be obtained when used <sup>LUMIRROR</sup> ~~Lumirror~~ X30 produced by Toray

Industries, Inc. The surface roughness of the non-adhering medium 801 was measured to be in a range of

- 15 0.1 nm to 2 nm in mean square, by using a three-dimensional surface roughness meter of <sup>a</sup> non-contact

optical system. In addition, reference numeral 802

indicates a material to be treated consisting of an

aluminum sheet having a length of 10 cm and a thickness of 0.5 mm.

- 20 The material 802 ~~to be treated~~ was fixed to a jig (not shown in the drawings) having a groove formed at a laser irradiation position, and a non-adhering medium 801 was placed on the material 802 ~~to be treated~~ at a position to be irradiated with laser light.

- 25 Subsequently, a presser jig (not shown in the drawings) having at a cutting position a groove to be penetrated by laser light <sup>was</sup> used to closely contact the non-



adhering medium 801 with the material 802 ~~to be treated~~  
<sup>at</sup> under 1 kg/cm<sup>2</sup> pressure. Subsequently, using Ar as a  
shield gas, the material to be treated was irradiated  
with laser light 800 along the groove to be penetrated  
by the light to cut the material 802. The irradiation  
conditions of the laser light 800 were as follows:  
outgoing energy: 25J; pulse width: 3 ms; pulse  
repetition speed: 15 PPS; laser beam diameter:  $\phi$ 0.5 mm.

The laser irradiated portion of the non-adhering  
medium 801 was melted and evaporated by the irradiation  
of laser light. Once cutting was completed ~~by using~~  
~~laser light~~, the presser jig was opened and the  
remaining non-adhering medium 801 was removed by using  
tweezers to complete the series of operations.  
Although <sup>in</sup> this example <sup>are used</sup> ~~used~~ the tweezers to remove the  
non-adhering medium 801, a method of blowing the medium  
off by ~~using~~ a shield gas may be suitably used.

Since in this example the non-adhering medium 801  
was placed on the laser light-irradiated surface of the  
material to be treated, the amount of energy required  
for cutting could be ~~remarkably~~ <sup>substantially</sup> reduced. Furthermore,  
since the non-adhering medium 801 is removed after  
laser irradiation, ~~no~~ <sup>the</sup> non-adhering medium 801 <sup>does not</sup> ~~remains~~  
after the series of operations have been finished,  
thereby avoiding appearance problems and preventing  
problems from occurring in the post-process.

This example <sup>teaches a</sup> ~~provides~~ stable laser treatment

because <sup>2</sup> [in this example,] <sup>the</sup> laser treatment can be  
carried out <sup>at a</sup> ~~with a~~ lower energy than ~~that of~~ the  
conventional techniques and the reflectance is  
determined <sup>by</sup> ~~depending on~~ the physical characteristics of

5 the placed non-adhering medium. In addition, the  
material is treated while holding the non-adhering  
medium, thereby enabling stable close contact and, thus,

W stable laser treatment. Furthermore, the operator ~~must~~ <sup>needs</sup>

<sup>to</sup>  
only place the non-adhering medium, thereby increasing

10 the treatment speed. In addition, since the non-

adhering medium can be easily removed after laser

treatment, the present example provides a laser

treatment method that avoids appearance problems, while <sup>also</sup>  
preventing problems ~~from occurring~~ in the post-process.

15 (Example 7)

<sup>was</sup>  
In This example, <sup>2</sup> ~~used~~ laser light <sup>to</sup> weld the  
electrodes of photovoltaic elements. <sup>2</sup> The electrodes  
<sup>ed</sup>  
consisting of a copper foil.

20 Figs. 18A and 18B and 19A to 19C are schematic  
views showing the appearance of a photovoltaic element  
module according to Example 7 of the present invention.

Fig. 18A is a plan view of a photovoltaic element as  
seen from its light-receiving surface, and Fig. 18B is  
a sectional view of the photovoltaic element shown in  
25 Fig. 18A, which is taken along the line 18B-18B in Fig.

18A. In addition, Fig. 19A is a plan view of two  
photovoltaic elements connected in series as seen from

their light-receiving surface, Fig. 19B is an enlarged view of the series-connected portion in Fig. 19A, and Fig. 19C is a sectional view of Fig. 19B. Fig. 20 is a schematic view showing the method of supplying non-adhering and anti-reflection materials according to Example 7.

In Fig. 18A, reference numeral 900 indicates a 300 mm x 280 mm photovoltaic element comprising a substrate 902, a lower electrode layer 903, a semiconductor layer 904 consisting of amorphous silicon and having a photovoltaic function, and an upper electrode layer 905.

In this example, the substrate for supporting the entire photovoltaic element comprises a <sup>150  $\mu$ m thick</sup> stainless steel plate ~~having a thickness of 150  $\mu$ m~~. An Al layer of about 2,000 Å ~~in thickness~~ and a ZnO layer of about 13,000 Å ~~in thickness~~ were sequentially formed on the substrate 902 as the lower electrode layer 903 by using the sputtering method. In addition, the semiconductor layer 904 was formed by sequentially stacking an n-, i-, p-, n-, i-, and p-type semiconductor layers in this order from the substrate side by using the plasma CVD method. The thicknesses of these layers were about 150 Å, 4,000 Å, 100 Å, 100 Å, 800 Å, and 100 Å, respectively. In addition, the upper electrode layer 905 was a transparent electrode consisting of a thin indium oxide film of about 700 Å in thickness, and was

formed by depositing In in an O<sub>2</sub> atmosphere by using the resistance heating method. Furthermore, to prevent an effective light-receiving area from being affected by the adverse effect of a short circuit between the substrate and the transparent electrode that may occur when the outer circumference of the photovoltaic element is cut, etching paste containing FeCl<sub>3</sub> or AlCl<sub>3</sub> was coated on a part of the upper electrode layer 905 by using screen printing, and was heated and washed to linearly remove the part of the upper electrode layer 905 to thereby form an etching line 901.

Subsequently, a copper foil strip having a width of 10 mm, a length of 285 mm, and a thickness of 100 μm was formed near one side (280 mm long) of the back surface (on the substrate 902 side) of the photovoltaic element as a back-surface-side conductive foil 909, by using the method disclosed in Japanese Patent Application Laid Open No. 8-139349. One side of the copper foil strip protruded out from the photovoltaic element, as shown in Fig. 18A.

Subsequently, an insulating adhesive tape 908 comprising polyimide as a base and having a width of 10 mm, a length of 280 mm, and a thickness of 50 μm was applied to one side of the front surface (on the upper electrode layer 905) of the photovoltaic element such that the tape 908 is opposed to the back-surface-side conductive foil 909.

Subsequently, a carbon-coating wire comprising a copper wire ~~of~~ <sup>and</sup> 100  $\mu\text{m}$  in diameter coated with carbon paste was formed on the front surface of the photovoltaic element as a collecting electrode 906. In this case, the carbon-coating wires were continuously formed on the upper electrode layer 905 and the insulating adhesive tape 908 at a pitch of 14 mm such that the wires crossed the insulating tape.

Furthermore, a front-surface-side conductive foil 907 that was a further collecting electrode different from the collecting electrode 906 was formed on the insulating adhesive tape 908. The front-surface-side conductive foil 907 was formed by placing a copper foil strip having a width of 10 mm, a length of 285 mm, and a thickness of 100  $\mu\text{m}$  on the insulating adhesive tape 908 with interposition of a part of the collecting electrode 906 therebetween and heating, pressurizing, fixing the strip at 200°C and 1 kg/cm<sup>2</sup> for 60 seconds. One side of the copper foil strip was protruded out from the photovoltaic element 900 on a side opposite to the back-surface-side conductive foil 909, as shown in Fig. 18A.

To use for electric power generation the photovoltaic element produced in this manner, a plurality of photovoltaic elements were electrically connected in series to produce a photovoltaic element module. The connection method is described in Figs.

19A to 19C.

As shown in Figs. 19A to 19C, two adjacent photovoltaic elements were arranged <sup>so</sup> ~~such~~ that a part of the front-surface-side conductive foil 907 of a photovoltaic element 1 overlapped a part of the back-surface-side conductive foil 909 of a photovoltaic element 2 over a distance of 3 mm.

Subsequently, a non-adhering medium 913 was placed on the overlapping laser-welded portion between a part of the front-surface-side conductive foil 907 of the photovoltaic element 1 and a part of the back-surface-side conductive foil 909 of the photovoltaic element 2. As the non-adhering medium 913, a commercially available magnetic tape was used, which comprises a magnetic substance, such as carbon black, coated or deposited on one side of polyethyleneterephthalate or polyethylenenaphthalate. This example used T-120VF produced by Sony Corporation, but the experiments conducted by the inventors confirmed that performance similar to that of this example can be obtained when used other magnetic tapes, such as P6-120HMP2 or VXST-120VF, produced by Sony Corporation, or NV-ST120XPZ or NV-TTC40HGK produced by Matsushita Electric Industrial Co., Ltd., or heat transfer ribbons, such as TL-12K produced by King Jim Co., Ltd., CF-PR190 produced by Matsushita Electric Industrial Co., Ltd., or JW-Z180 produced by Toshiba Corporation. Since these magnetic

tapes are supplied <sup>in a</sup> ~~from the~~ form of a roll, <sup>a</sup> ~~the~~  
subsequent laser treatment can be prepared by <sup>2</sup> ~~after~~  
~~laser treatment~~ <sup>2</sup> releasing the presser jig and feeding  
<sup>after each laser treatment</sup> the tape forward. In addition, the surface roughness  
5 of the magnetic surfaces of these magnetic tapes was  
measured to be in a range of 5 nm to 20 nm in mean  
square.

Furthermore, a presser jig (not shown in the  
drawings) was used to press the magnetic tape <sup>that</sup> ~~which~~ was  
10 the non-adhering medium 913 at 10 kg/cm<sup>2</sup> with the  
magnetic surface facing the front-surface-side  
conductive foil 907 of the photovoltaic element 1 <sup>1</sup> ~~which~~  
was a material to be treated.

Then, the overlapping portion between the front-  
15 surface-side conductive foil 907 of the photovoltaic  
element 1 and the back-surface-side conductive foil 909  
of the photovoltaic element 2 <sup>2</sup> ~~which~~ was pressed by the  
presser jig, was irradiated with laser light to carry  
out welding and mechanically and electrically connect  
20 the elements to each other. Reference numeral 910  
designates a welding point. As the laser for providing  
a high energy enough to weld a metal, it is possible to  
use a YAG laser, a phosphate glass laser, a silicate  
glass laser, or a CO<sub>2</sub>-laser-excited far infrared laser.  
25 In particular, the YAG laser has excellent  
characteristics <sup>g</sup> such as its capability of transmitting  
laser light through optical fibers to enable treatment

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at a position remote from the laser oscillator, and enables the welding condition to be changed by the selection of the optical fibers and an outgoing unit. Another excellent characteristic of this laser is its capability of dividing a laser light into 2 to about 10 beams.

*For* This example *was* used the YAG laser *A* to execute welding under the following conditions: outgoing energy: 6J; pulse width: 5 ms *10* laser diameter: 0.6 mm; number of welding points: 12.

The method of supplying the magnetic tape as the non-adhering medium 913 according to this example is described with reference to Fig. 20. In this figure, reference numeral 920 indicates a magnetic tape housed in a cassette, 921 a reel around which a magnetic tape irradiated with laser light is wound, and 922 a presser member for pressing the magnetic tape 913 against a junction portion between the front-surface-side conductive foil 907 of the photovoltaic element 1 and the back-surface-side conductive foil 909 of the photovoltaic element *2* which are materials to be treated. A transfer means (not shown in the drawings) is used to transfer to a laser treatment position the front-surface-side and back-surface-side conductive foils 907 and 909 of the photovoltaic elements 1 and 2, respectively. Then, the presser jig 922 presses the magnetic tape 913 against the junction portion between

the front-surface-side conductive foil 907 of the photovoltaic element 1 and the back-surface-side conductive foil 909 of the photovoltaic element 2. Subsequently, the junction portion is irradiated with laser light 930 to carry out a predetermined laser treatment.

The portion of the magnetic tape 913 irradiated with laser light <sup>melts</sup> ~~is melted~~ <sup>is</sup> and evaporated by the heat generated by welding. Furthermore, since a magnetic substance having a surface roughness of 5 nm to 20 nm in mean square is coated or deposited on the surface of the magnetic tape 913 closely contacting the front-surface-side conductive foil 907 of the photovoltaic element 1, after welding, the magnetic tape 913 can be removed by simply releasing the presser jig. The magnetic tape 913 may adhere to the front-surface-side conductive foil 907 in some cases, <sup>but</sup> ~~the tape~~ can be easily removed by applying <sup>a</sup> force ~~enough~~ to slightly release the tape from the foil (not shown in the drawings).

Subsequently, the magnetic tape 913 is fed by 3 cm ~~so as~~ to be wound around the winding reel 921, and an unused magnetic tape is supplied from the magnetic tape cassette 920 to complete preparations for the subsequent laser treatment. The treated photovoltaic elements 1 and 2 are conveyed out by a transfer means (not shown in the drawings) immediately after laser

treatment.

The electric resistance of the laser welded portion was measured to be  $0.013 \Omega$ . With respect to the performance of the photovoltaic element 900, the effective area was  $809.0 \text{ cm}^2$ , the generated current was 5.38 A, the generated voltage was 1.2 V, and the generated power was 6.45 W, therefore the resistance loss of the laser welded portion was 0.9 mW, which is only 0.015% of the generated electric power of 6.45 W.

In addition, the tensile strength of the laser welded portion was measured to be in a range of 8 kg to 15 kg.

In this example, with respect to the time required for laser welding, 2.0 seconds were required to feed-in and positioning of the photovoltaic elements 1 and 2, 3.5 seconds were required for welding (including the movement of the laser beam outgoing tip), and 1.0 second was required for feed-out of the treated elements. Thus, the connection of the two photovoltaic elements was completed in 6.5 seconds.

That is, this example can provide a method of connecting photovoltaic elements in series that enables laser welding with a lower energy than ~~that of~~ the conventional techniques, ~~that~~ enables high speed treatment, and ~~that~~ avoids appearance problems while preventing problems occurring in the post-process.

The present invention minimizes the time required

for heating when executed to connect a group of  
photovoltaic elements, thereby preventing the  
components of the photovoltaic elements, such as the  
semiconductor layer and conductive adhesive, from being  
5 degraded by wide-ranging heating.

In addition, in the present invention, each  
operation can be completed in a short time to enable  
mass production.

Furthermore, the present invention eliminates the  
10 needs for solder to avoid reduction of the production  
yield due to solder residues and <sup>to</sup> avoid the adverse  
effect of remaining fluxes on a covering material.

In addition, the present invention <sup>teaches using</sup> ~~uses~~ the color  
ink or film to easily increase the laser absorption  
15 efficiency, thereby providing an inexpensive  
photovoltaic element production method having a high  
production efficiency.

Furthermore, in the method of placing the non-  
adhering medium on the surface to be irradiated with  
20 laser light of the material to be treated, and  
irradiating the non-adhering medium with laser light  
while holding the non-adhering medium and the material,  
laser treatment can be stably executed because the  
reflectance is determined depending on the physical  
25 properties of the placed material (non-adhering  
medium). In addition, the treatment can be carried out  
while holding the non-adhering medium and the material



only placing

What is claimed is:

1. A photovoltaic element module comprising at least two electrically connected photovoltaic elements to each other, wherein a medium capable of absorbing at least 10% or more of a light having a wavelength of 0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$  is provided on an electric connection portion of the photovoltaic element.
2. A photovoltaic element module according to Claim 1, wherein the photovoltaic element has at least a conductive substrate and a semiconductor layer.
3. A photovoltaic element module according to Claim 1, wherein the medium is a color ink.
4. A photovoltaic element module according to Claim 1, wherein the medium is a film having a thickness of 5  $\mu\text{m}$  to 30  $\mu\text{m}$ .
5. A photovoltaic element module according to Claim 1, wherein the medium consists of at least one of Fe, Ni, and solder.
6. A photovoltaic element module according to Claim 1, wherein the medium absorbs 10% or more of a laser light having a wavelength of 1.06  $\mu\text{m}$ .

7. A photovoltaic element module according to Claim 1, wherein in the electric connection portion, each of metal members provided on each of the photovoltaic elements are electrically connected to each other.

8. A photovoltaic element module according to Claim 7, wherein the metal members comprise at least one of gold, silver, copper, stainless, and aluminum as a main component.

9. A method of producing a photovoltaic element module, which comprises a step of electrically connecting at least two photovoltaic elements to each other, wherein the step is a step of electrically connecting a first and a second photovoltaic elements by providing on a part of the first photovoltaic element a medium capable of absorbing at least 10% or more of a light having a wavelength of 0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$  and irradiating the medium with a laser light having a wavelength of 0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$ .

10. A method of producing a photovoltaic element module according to Claim 9, wherein the medium is a color ink.

11. A method of producing a photovoltaic element



module according to Claim 9, wherein the medium is a film having a thickness of 5 mm to 30 $\mu$ m.

12. A method of producing a photovoltaic element  
5 module according to Claim 9, wherein the medium consists of at least one of Fe, Ni, and solder.

13. A method of producing a photovoltaic element  
10 module according to Claim 9, wherein a metal member is provided on an electrode portion of the photovoltaic element and wherein the medium is provided on a surface of the metal member.

14. A method of producing a photovoltaic element  
15 module, which comprises a step of electrically connecting at least two photovoltaic elements to each other, wherein each of the photovoltaic element has at least a conductive substrate, a semiconductor layer, and a light-transmissive electrode, and wherein the  
20 step is a step of electrically connecting a conductive substrate of a first photovoltaic element and a light-transmissive electrode of a second photovoltaic element to each other by laser welding.

15. A method of producing a photovoltaic element  
25 module according to Claim 14, wherein a metal member is are provided on the conductive substrate of the first

photovoltaic element and/or the light-transmissive  
electrode of the second photovoltaic element, wherein a  
medium capable of absorbing a laser light is provided  
on the metal member, and wherein the medium is  
5 irradiated with the laser light to carry out the laser  
welding.

16. A method of producing a photovoltaic element  
module according to Claim 15, wherein the medium  
10 absorbs 10% or more of a light having a wavelength of  
0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$ .

17. A non-contact treatment method of carry out  
treatment by using an energy supply means for supplying  
15 energy, which comprises placing a non-adhering medium  
capable of absorbing the energy on a material to be  
treated, and irradiating the non-adhering medium with  
the energy.

20 18. A non-contact treatment method according to  
Claim 17, wherein a surface of the non-adhering medium  
closely contacting the material to be treated has a  
surface roughness of 0.1 nm to 5,000 nm in mean square.

25 19. A non-contact treatment method according to  
Claim 17, wherein the non-adhering medium has at least  
a polymer film.

20. A non-contact treatment method according to Claim 17, wherein the non-adhering medium is a magnetic tape.

5           21. A non-contact treatment method according to Claim 20, wherein a magnetic surface of the magnetic tape is closely contacted with the material to be treated.

10           22. A non-contact treatment method according to Claim 17, wherein the non-adhering medium absorbs 10% or more of a light having a wavelength of 0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$ .

15           23. A non-contact treatment method according to Claim 17, wherein the energy is light, heat, or electromagnetic waves.

20           24. A non-contact treatment method according to Claim 17, wherein the non-adhering medium is irradiated with the energy while pressing the non-adhering medium against the material to be treated.

25           25. A non-contact treatment method according to Claim 17, wherein the non-adhering medium is removed by irradiation of the energy.

26. A non-contact treatment method according to Claim 17, wherein the non-adhering medium is removed after the energy irradiation.

5           27. A non-contact treatment method according to Claim 17, wherein the treatment is cutting or welding.

10           28. A non-contact treatment method according to Claim 17, wherein the non-adhering medium is supplied from a roll of the non-adhering medium, and after the energy irradiation, is wound up.

15           29. A non-contact treatment method according to Claim 17, wherein the material to be treated is an electrode of an electric part.

20           30. A non-contact treatment method according to Claim 17, wherein the material to be treated is an electrode of a photovoltaic element.

25           31. A non-contact treatment method according to Claim 17, wherein the material to be treated is a material having a high reflectance with respect to energy irradiation.

32. A method of producing a photovoltaic element module, which comprises a step of electrically

connecting at least two photovoltaic elements to each other, wherein the step is a step of placing on a part of a first photovoltaic element a non-adhering medium capable of absorbing energy and irradiating the medium with energy to electrically connect the first photovoltaic element and a second photovoltaic element to each other.

33. A method of producing a photovoltaic element module according to Claim 32, wherein a surface of the non-adhering medium closely contacting a material to be treated has a surface roughness of 0.1 nm to 5,000 nm in mean square.

34. A method of producing a photovoltaic element module according to Claim 32, wherein the non-adhering medium has at least a polymer film.

35. A method of producing a photovoltaic element module according to Claim 32, wherein the non-adhering medium is a magnetic tape.

36. A method of producing a photovoltaic element module according to Claim 35, wherein a magnetic surface of the magnetic tape is closely contacted with a part of the first photovoltaic element.

37. A method of producing a photovoltaic element module according to Claim 32, wherein the non-adhering medium absorbs 10% or more of a light having a wavelength of 0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$ .

5

38. A method of producing a photovoltaic element module according to Claim 32, wherein a metal member is provided on an electrode portion of the photovoltaic element and wherein the non-adhering medium is provided on a surface of the metal member.

39. A photovoltaic element module produced by the method of Claim 32 of producing a photovoltaic element module.

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# Abstract of Disclosure

Before electrically connecting at least two photovoltaic elements, a medium capable of absorbing at least 10% or more of a light having a wavelength of 0.4  
5  $\mu\text{m}$  to 2.0  $\mu\text{m}$  is provided on an electric connection portion of the photovoltaic element, whereby the present invention provides a method of electrically connecting a group of photovoltaic elements to one another with a high yield and easy automatization.

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TECHNICAL FIELD